

# THE UTILIZATION OF 3X3 MATRICES IN SETTING KINEMATICS CHAINS ANALYSIS FOR ROBOTS COMPONENTS

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## ABSTRACT

*Within the kinematic study of a rigid solid, its motion is studied face-to-face by a reference system, fixing positions, speeds and accelerations of a reference system, solidarily connected to the rigid solid.*

KEYWORDS: kinematics, analysis, chains, transformation matrix.

### 1. Introduction

The author considers, in this paper, the rotation of the rigid solid around a certain axis  $(\Delta)$ , with an angle  $\varphi$  (Figure 1). The motion of a solid rigid is studied face-to-face by a reference system with fixing position.

### 2. Description method of analysis

We deem the rotation axis  $(\Delta)$ , defined face-to-face by a tri-orthogonal system  $O_0x_0y_0z_0$ , which is fixedly connected with the direction cosines

$$\alpha_{11} = \cos \alpha, \alpha_{12} = \cos \beta, \alpha_{13} = \cos \gamma; \quad (1)$$

and the reference system  $O_1x_1y_1z_1$ , whose axis  $O_1x_1$  coincides with the rotation axis  $(\Delta)$ , and the axis  $O_1z_1$  is situated in  $O_0x_0z_0$  plan.

The positions of the reference system axis  $O_1x_1y_1z_1$  are defined in connection with a system fixedly connected by

$$\begin{aligned} O_1x_1 : \alpha_{11}^l &= \cos \alpha, \alpha_{12}^l = \cos \beta, \alpha_{13}^l = \cos \gamma \\ O_1y_1 : \alpha_{21}^l &= \cos \alpha_2, \alpha_{22}^l = \cos \beta_2, \alpha_{23}^l = \cos \gamma_2 \\ O_1z_1 : \alpha_{31}^l &= \cos \alpha_3, \alpha_{32}^l = \cos \beta_3, \alpha_{33}^l = \cos \gamma_3 \end{aligned} \quad (2)$$

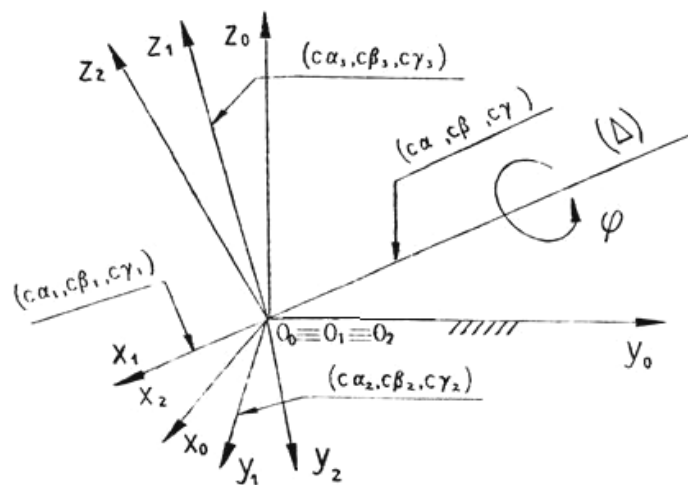


Figure 1. Rotation of the rigid solid around a certain axis  $(\Delta)$ , with an angle  $\varphi$

The transformation matrix from the reference system  $O_1x_1y_1z_1$  to the fixedly reference system is:

$$[a_{10}]^T = \begin{bmatrix} \alpha_{11} & \alpha_{21} & \alpha_{31} \\ \alpha_{12} & \alpha_{22} & \alpha_{32} \\ \alpha_{13} & \alpha_{23} & \alpha_{33} \end{bmatrix} = \begin{bmatrix} \cos \alpha_1 & \cos \alpha_2 & \cos \alpha_3 \\ \cos \beta_1 & \cos \beta_2 & \cos \beta_3 \\ \cos \gamma_1 & \cos \gamma_2 & \cos \gamma_3 \end{bmatrix}, \quad (3)$$

respectively from the fixedly reference system  $O_0x_0y_0z_0$  to the reference system  $O_1x_1y_1z_1$ :

$$[a_{10}] = \begin{bmatrix} \alpha_{11} & \alpha_{12} & \alpha_{13} \\ \alpha_{21} & \alpha_{22} & \alpha_{23} \\ \alpha_{31} & \alpha_{32} & \alpha_{33} \end{bmatrix} = \begin{bmatrix} \cos \alpha_1 & \cos \beta_1 & \cos \gamma_1 \\ \cos \alpha_2 & \cos \beta_2 & \cos \gamma_2 \\ \cos \alpha_3 & \cos \beta_3 & \cos \gamma_3 \end{bmatrix}, \quad (4)$$

Using the relations that express the perpendicularity conditions of two axes, we can write

$$\cos \alpha_1 \cos \beta_1 + \cos \alpha_2 \cos \beta_2 + \cos \alpha_3 \cos \beta_3 = 0 \quad (5)$$

$$\cos \beta_1 \cos \gamma_1 + \cos \beta_2 \cos \gamma_2 + \cos \beta_3 \cos \gamma_3 = 0$$

in which, replacing

$$\begin{aligned} \cos \alpha_1 &= \cos \alpha; \cos \beta_1 = \cos \beta; \\ \cos \gamma_1 &= \cos \gamma; \cos \beta_3 = 0; \cos \beta_2 = \sin \beta \end{aligned} \quad (6)$$

results:

$$\begin{aligned} \cos \alpha \cos \beta + \cos \alpha_2 \sin \beta &= 0 \\ \Rightarrow \cos \alpha_2 &= -\frac{\cos \alpha \cos \beta}{\sin \beta} \end{aligned} \quad (7)$$

$$\begin{aligned} \cos \beta \cos \gamma + \sin \beta \cos \gamma_2 &= 0 \\ \Rightarrow \cos \gamma_2 &= -\frac{\cos \beta \cos \gamma}{\sin \beta} \end{aligned}$$

Having in view the fact that each element of the transformation matrix can be equal to its cofactor, results:

$$\begin{aligned} \cos \alpha_3 &= \cos \beta_1 \cos \gamma_2 - \cos \gamma_1 \cos \beta_2 = \\ &= -\frac{\cos^2 \beta \cos \gamma}{\sin \beta} - \cos \gamma \sin \beta = -\frac{\cos \gamma}{\sin \beta} \end{aligned} \quad (8)$$

$$\begin{aligned} \cos \gamma_3 &= \cos \alpha_1 \cos \beta_2 - \cos \beta_1 \cos \alpha_2 = \\ &= \cos \alpha \sin \beta + \frac{\cos \alpha \cos^2 \beta}{\sin \beta} = \frac{\cos \alpha}{\sin \beta} \end{aligned}$$

We deem the rotation of a  $\varphi$  angle system  $O_1x_1y_1z_1$  around the  $O_1x_1 \equiv (\Delta)$  axis. In this case, the transformation matrix becomes

$$[R_{0x}^\varphi] = [a_{21}]^T = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \varphi & -\sin \varphi \\ 0 & \sin \varphi & \cos \varphi \end{bmatrix}. \quad (9)$$

Considering a point  $M'$  defined in  $O_2x_2y_2z_2$  system, by vector  $(r_{M'}^2)$ , it results from the rotation of  $\varphi$  around its axis  $(\Delta)$ , from the point  $M$  belonging to the  $O_1x_1y_1z_1$  system, by vector  $(r_M^1)$ .

Knowing that the analytic expression of the position vector is invariable face-to-face by rotation of the coordinating axis, we can write:

$$(r_{M'}^2) = (r_M^1) \quad (10)$$

whence the result of left multiplying by  $[a_{21}]^T$ , is:

$$[a_{21}]^T (r_{M'}^2) = [a_{21}]^T (r_M^1). \quad (11)$$

We go on writing that

$$(r_{M'}^0) = [a_{10}]^T (r_{M'}^1) \quad (12)$$

$$(r_M^0) = [a_{10}]^T (r_M^1) \quad (13)$$

which by  $[a_{10}]$  left multiplying there results:

$$(r_{M'}^1) = [a_{10}] (r_M^0), \quad (14)$$

$$(r_M^I) = [a_{10}] (r_M^0) \quad (15)$$

If we replace (14) and (15) in (11), the result is shown in:

$$[a_{21}]^T (r_{M'}^2) = [a_{21}]^T [a_{10}] (r_M^0) \quad (16)$$

whence by  $[a_{10}]^T$  left-multiplying, results:

$$[a_{10}]^T [a_{21}]^T (r_{M'}^2) = [a_{10}]^T [a_{21}]^T [a_{10}] (r_M^0). \quad (17)$$

Seeing that

$$(r_{M'}^0) = [a_{10}]^T [a_{21}]^T (r_{M'}^2), \quad (18)$$

the relation (17) becomes

$$(r_{M'}^0) = [a_{10}]^T [a_{21}]^T [a_{10}] (r_M^0) \quad (19)$$

and the transformation matrix is

$$[a_r]^T = [a_{10}]^T [a_{21}]^T [a_{10}]. \quad (20)$$

The matrix  $[a_r]$ , defined by the relation (20), define the rotation of the rigid solid around the axis  $(\Delta)$ , with an angle  $\varphi$ , face-to-face by the reference system fixedly connected.

Calculating the matrix products

$$\begin{aligned} [a_{10}]^T [a_{21}]^T &= \\ &= \begin{bmatrix} c\alpha & -c\alpha \frac{c\beta}{s\beta} & -\frac{c\gamma}{s\beta} \\ c\beta & s\beta & 0 \\ c\gamma & -c\beta \frac{c\gamma}{s\beta} & \frac{c\alpha}{s\beta} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\varphi & -s\varphi \\ 0 & s\varphi & c\varphi \end{bmatrix} = \\ &= [a_{20}]^T \end{aligned} \quad (21)$$

and

$$\begin{aligned} [a_{20}]^T [a_{10}] &= \\ &= \begin{bmatrix} c\alpha & -\frac{c\alpha c\beta c\varphi + c\gamma s\varphi}{s\beta} & \frac{-c\gamma c\varphi + c\alpha c\beta s\varphi}{s\beta} \\ c\beta & s\beta c\varphi & -s\beta s\varphi \\ c\gamma & \frac{c\alpha s\varphi - c\beta c\gamma c\varphi}{s\beta} & \frac{c\beta c\gamma s\varphi + c\alpha c\varphi}{s\beta} \end{bmatrix} \times \\ &\times \begin{bmatrix} \frac{c\alpha}{s\beta} & c\beta & -\frac{c\gamma}{s\beta} \\ \frac{c\alpha c\beta}{s\beta} & s\beta & -\frac{c\beta c\gamma}{s\beta} \\ -\frac{c\varphi}{s\beta} & 0 & \frac{c\alpha}{s\beta} \end{bmatrix} \end{aligned} \quad (22)$$

finally, the transformation matrix the relation becomes:

$$\begin{aligned} [a_r]^T &= [a_{10}]^T [a_{21}]^T [a_{10}] = \\ &= \begin{bmatrix} \alpha_{11}^r & \alpha_{21}^r & \alpha_{31}^r \\ \alpha_{12}^r & \alpha_{22}^r & \alpha_{32}^r \\ \alpha_{13}^r & \alpha_{23}^r & \alpha_{33}^r \end{bmatrix}, \end{aligned} \quad (23)$$

where

$$\begin{aligned} \alpha_{11}^r &= c^2 \alpha + \\ &+ \frac{c^2 \alpha c^2 \beta c \gamma + c \alpha c \beta c \gamma s \varphi - c \alpha c \beta c \gamma s \varphi + c^2 \gamma c \varphi}{s^2 \beta} \end{aligned}$$

$$\alpha_{21}^r = c \alpha c \beta - \frac{s \beta c \varphi c \alpha c \beta}{s \beta} + \frac{s \beta c \gamma s \varphi}{s \beta}$$

$$\alpha_{31}^r = c \gamma c \alpha - \frac{c^2 \alpha c \beta s \varphi}{s^2 \beta} + \frac{c \alpha c^2 \beta c \gamma c \varphi}{s^2 \beta} -$$

$$- \frac{c \beta c^2 \gamma s \varphi + c \alpha c \gamma c \varphi}{s^2 \beta}$$

$$\alpha_{12}^r = c \alpha c \beta - \frac{c \alpha c \beta s \beta c \varphi + c \gamma s \beta s \varphi}{s \beta}$$

$$\alpha_{22}^r = c^2 \beta + s^2 \beta c \varphi$$

$$\alpha_{32}^r = c \gamma c \beta + \frac{c \alpha s \beta s \varphi - c \beta s \beta c \gamma c \varphi}{s \beta}$$

$$\begin{aligned} \alpha_{13}^r &= c \alpha c \gamma + \\ &+ \frac{c \alpha c^2 \beta c \gamma c \varphi + c \beta c^2 \gamma s \varphi - c \alpha c \gamma c \varphi + c^2 \alpha c \beta s \varphi}{s^2 \beta} \end{aligned}$$

$$\alpha_{23}^r = c \beta c \gamma - \frac{s \beta c \beta c \gamma c \varphi}{s \beta} - \frac{s \beta c \alpha s \varphi}{s \beta}$$

$$\alpha_{33}^r = c^2 \gamma - \frac{c \alpha c \beta c \gamma s \varphi}{s^2 \beta} + \frac{c^2 \beta c^2 \gamma c \varphi}{s^2 \beta} +$$

$$+ \frac{c \beta c \gamma c \alpha s \varphi + c^2 \alpha c \varphi}{s^2 \beta}.$$

If the  $(\Delta)$  axis versor is written down  $(u)$ ,

$$\begin{aligned} (u) &= [c\alpha \quad c\beta \quad c\gamma]^T = \\ &= [u_x \quad u_y \quad u_z]^T \text{ and } v\varphi = 1 - c\varphi, \end{aligned} \quad (24)$$

we get the form given in eq.(2)

$$[a_r]^T = \begin{bmatrix} u_x u_x v\varphi + c\varphi & u_y u_x v\varphi - u_z s\varphi & u_z u_x v\varphi + u_y s\varphi \\ u_x u_y v\varphi + u_z s\varphi & u_y u_y v\varphi + c\varphi & u_z u_y v\varphi - u_x s\varphi \\ u_x u_z v\varphi - u_y s\varphi & u_y u_z v\varphi + u_x s\varphi & u_z u_z v\varphi + c\varphi \end{bmatrix}. \quad (25)$$

Having the rotation matrix, we can determine the direction cosines and the rotation angle:

$$\varphi = \arccos \frac{\alpha_{11} + \alpha_{22} + \alpha_{33} - 1}{2}; \quad (26)$$

$$(u) = \frac{1}{2s\varphi} \begin{bmatrix} \alpha_{23}^r - \alpha_{32}^r \\ \alpha_{31}^r - \alpha_{13}^r \\ \alpha_{12}^r - \alpha_{21}^r \end{bmatrix}. \quad (27)$$

### 3. Conclusions

Using the method presented in the previous section the next conclusions result:

- a) The presented solution is proper to the calculation of the  $\varphi$  angle with values between  $0^\circ$  and  $180^\circ$ . If  $\varphi = 0^\circ$  or  $180^\circ$ , the solution is undefined regarding the position of the rotation axis;
- b) When the vector  $(u)$  isn't a unitary vector it must be normalized, finding in such a way its components face-to-face by the fixedly reference system.

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